

Çankaya University
 Electrical & Electronics Engineering Department
 Solutions to EE 322 Energy Distribution Homework 1 and 2

HW1-1

$$(a) \quad GMR = \sqrt[9]{\left[\left(e^{-\frac{1}{4}r} \right) (2r)(2r) \right]^3} = r \sqrt[3]{4e^{-\frac{1}{4}}} \\ = \underline{\underline{1.4605 r}}$$

$$(b) \quad GMR = \sqrt[16]{\underbrace{\left[\left(e^{-\frac{1}{4}r} \right) (2r)(4r)(6r) \right]^2}_{\text{Distances for each outer conductor}} \underbrace{\left[\left(e^{-\frac{1}{4}r} \right) (2r)(2r)(4r) \right]^2}_{\text{Distances for each inner conductor}}} \\ GMR = \sqrt[16]{\left(e^{-\frac{1}{4}} \right)^4 (2)^6 (4)^4 (6)^2 (r)} = \underline{\underline{2.1554r}}$$

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$$\begin{aligned}
 \text{(c) } GMR &= r \sqrt[81]{\left[\underbrace{\left(e^{-\frac{1}{4}} \right) (2)^2 (4)^2 (\sqrt{20})^2 (\sqrt{8}) (\sqrt{32})}_{\text{Distances for each corner conductor}} \right]^4 \times \left[\underbrace{\left(e^{-\frac{1}{4}} \right) (2)^3 (\sqrt{8})^2 (\sqrt{20})^2 (4)}_{\text{Distances for each outside non-corner conductor}} \right]^4} \\
 &\quad \times \left[\underbrace{\left(e^{-\frac{1}{4}} \right) (2)^4 (\sqrt{8})^4}_{\text{Distances for the center conductor}} \right] \\
 GMR &= r \sqrt[81]{\left(e^{-\frac{1}{4}} \right)^9 (2)^{24} (\sqrt{8})^{16} (\sqrt{20})^{16} (4)^{12} (\sqrt{32})^4} \\
 GMR &= \underline{\underline{2.6374r}}
 \end{aligned}$$

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$$D_{AB} = \sqrt[9]{(6.1)^2 (6.2)^2 (6.3)6(6.05)(6.15)(6.25)} = 6.15\text{m}$$

The geometric mean radius of the equilateral arrangement of line A is

$$R_A = \sqrt[9]{(0.015576)^3 (0.1)^6} = 0.0538\text{m}$$

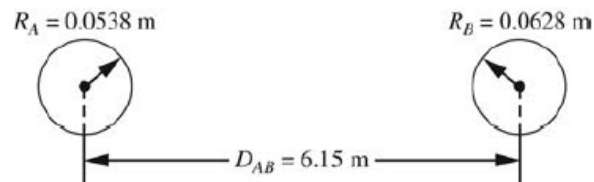
In which the first term beneath the radical is obtained from

$$r' = 0.7788 \quad r = 0.7788(0.02) = 0.015576\text{m}$$

The geometric mean radius of the line B is calculated below as per its configuration:

$$R_B = \sqrt[9]{(0.015576)^3 (0.1)^4 (0.2)^2} = 0.0628\text{m}$$

The actual configuration can now be replaced by the two equivalent hollow conductors each with its own geometric mean radius and separated by the geometric mean distance as shown below:



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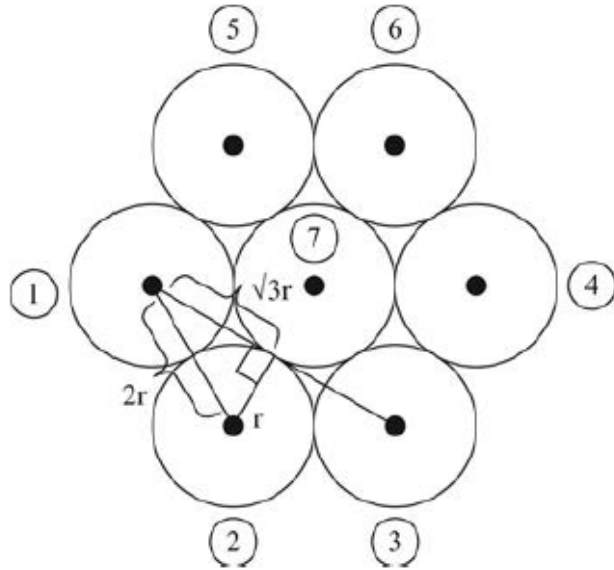
For each of six outer conductors:

$$D_{11} = r' = e^{-\frac{1}{7}} r$$

$$D_{12} = D_{16} = D_{17} = 2r$$

$$D_{13} = D_{15} = 2\sqrt{3}r$$

$$D_{14} = 4r$$



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(a) The total line inductance is given by

$$\begin{aligned}L_T &= \left[4 \times 10^{-4} \ln \frac{D}{r'} \right] \text{mH/m} \\ &= 4 \times 10^{-4} \ln \frac{3.6}{(0.7788)(0.023)} = 0.0021 \text{mH/m}\end{aligned}$$

(b) The total line reactance is given by

$$\begin{aligned}X_T &= 2\pi(60)4 \times 10^{-4} \ln \frac{D}{r'} \\ &= 0.1508 \ln \frac{D}{r'} \Omega/\text{km} \\ \text{or} \quad &0.2426 \ln \frac{D}{r'} \Omega/\text{mi}\end{aligned}$$

$$\therefore X_T = 0.787 \Omega/\text{km} \text{ or } 1.266 \Omega/\text{mi}$$

$$(c) \quad L_T = 4 \times 10^{-4} \ln \frac{7.2}{0.7788(0.025)} = 0.002365 \text{ mH/m}$$

Doubling the separation between the conductors causes only about a 13% rise in inductance.

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HW2-2

$$D_{eq} = \sqrt[3]{10 \times 10 \times 20} = 12.6 \text{ m}$$

$$D_s = (0.0435 \text{ ft}) \frac{1 \text{ m}}{3.28 \text{ ft}} = 0.0133 \text{ m}$$

$$\begin{aligned} X_1 &= \omega L_1 = 2\pi(60)2 \times 10^{-7} \ln\left(\frac{12.6}{0.149}\right) \frac{\Omega}{\text{m}} \times \frac{1000 \text{ m}}{1 \text{ km}} \\ &= 0.335 \Omega / \text{km} \end{aligned}$$

HW2-3

$$D_{eq} = \sqrt[3]{10 \times 10 \times 20} = 12.6 \text{ m}$$

$$r = \frac{1.293}{2} \ln\left(\frac{0.0254 \text{ m}}{1 \text{ in}}\right) = 0.01642 \text{ m}$$

$$D_{sc} = \sqrt[3]{rd^2} = \sqrt[3]{0.01642(0.5)^2} = 0.16 \text{ m}$$

$$C_1 = \frac{2\pi\epsilon_0}{\ln\frac{D_{eq}}{D_{sc}}} = \frac{2\pi(8.854 \times 10^{-12})}{\ln\left(\frac{12.6}{0.16}\right)} = 1.275 \times 10^{-11} \text{ F/m}$$

$$\bar{Y}_1 = j\omega C_1 = j2\pi(60)1.275 \times 10^{-11}(1000) = j4.807 \times 10^{-6} \text{ S/km}$$

$$Q_1 = V_{LL}^2 Y_1 = (500)^2 4.807 \times 10^{-6} = 1.2 \text{ MVAR/km}$$